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# Active thermography inspection of surface-whitened mortars – measurement of surface spectral absorptivity for investigation of efficient heating light wavelengths

Masashi Ishikawa<sup>a\*</sup>, Akira Emoto<sup>b</sup>, Yoshihiro Suto<sup>a</sup>, Hideo Nishino<sup>a</sup>

<sup>a</sup> Graduate School of Technology, Industrial and Social Sciences, Tokushima University,

2-1 Minamijosanjima, Tokushima, 770-8506, Japan

<sup>b</sup> Institute of Post-LED Photonics, Tokushima University, 2-1 Minamijosanjhma, Tokushima 770-8506, Japan

\*Corresponding author. Email: m.ishikawa@tokushima-u.ac.jp

# Abstract

The surface spectral absorptivity of surface-whitened mortars due to the occurrence of efflorescence (i.e., mortars whose surface was covered with calcium carbonate) was measured, and the relationship between the spectral absorptivity and inspection capability of active thermography inspection was investigated. The spectral absorptivity of mortars increased significantly at a wavelength of approximately 3000 nm regardless of the presence/absence of the discoloration. Experiments for mortar specimens using optical lights with wavelengths in the visible, short wavelength, and medium/long wavelength ranges showed that the heating efficiency and defect detection capability of active thermography inspection were correlated with the surface spectral absorptivity, and were higher when long wavelength light was used as a heater. Defects in the surface-whitened mortar specimen were detected more efficiently when the specimen was heated using a  $CO_2$  laser, whose wavelength is in the long wavelength range.

# Keywords

Non-destructive inspection; Infrared thermography; Spectral measurement; Concrete; Efflorescence

#### 1. Introduction

Infrared active thermography is a promising non-destructive inspection method. In this method, an inspection object is artificially heated, and the surface temperature during or after heating is observed using an infrared camera. For heating the inspection object, various methods, such as using optical lamps [1–4], air heaters [5, 6], laser heating [7–9], ultrasound [10–12], eddy current [13–15], etc., have been reported in many works. Among these methods, surface heating using optical lamps is one of frequently used methods for the inspection of structural components or for laboratory tests. When there is a defect in the object (e.g., a crack or delamination), the heat flow from the surface is disturbed by the defect, causing a local temperature irregularity around the defect. The defect is then identified by detecting the temperature abnormality in the thermal image obtained using the infrared camera. This method is non-contact and can easily inspect a wide area; thus, it is used for the inspection of various objects, including civil structures [16–19], mechanical components [20-23], composite materials [24-27], and additive manufactured components [28, 29]. However, the observed temperature is easily affected by the spectral characteristics of the inspected object surface, which can also affect the inspection results. For example, when inspecting concrete structures, the discoloration of the concrete surface can be an obstacle to thermographic inspection. Concrete surfaces can be blackened or whitened depending on those conditions. Surface blackening is caused in a polluted (or dusty) environment or by the growth of black crust. Surface whitening, on the other hand, is mainly caused by the occurrence of efflorescence [30, 31]. Efflorescence is the deposition of salts migrated from the interior of the mortar; in many cases, its major components is calcium carbonate caused by the reaction of calcium hydroxide in the mortar with carbon dioxide in the air. The occurrence of efflorescence can be a greater obstacle in active thermography inspections than the surface blacking; because it is a white deposit, visible and near-visible light should reduce absorptivity. The reduction of the absorptivity leads to the reduction of the input heat in active thermography, resulting in the deterioration of its inspection capability [32, 33].

This study focuses on the inspection of surface-whitened mortars and investigates the relationship between the surface spectral absorptivity and the inspection capability of active thermography inspection. First, the spectral absorptivity of whitened mortar specimens simulating the discoloration caused by efflorescence was measured using spectrometers. Subsequently, to verify the measured spectral absorptivity, the specimens were heated using optical lights with different wavelengths, and the heating efficiencies caused by the different lights were compared.

Finally, mortar specimens with an artificial defect were inspected by active thermography using an optical lamp or laser, and the relationship between the wavelength of the incident light and defect detection capability was examined. From the obtained results, the wavelengths of heating light efficient for active thermography inspection of discolored mortars were investigated.

# 2. Measurement of surface spectral absorptivity

Spectral measurements were performed to investigate the spectral absorptivity of incident light into mortars.

## 2.1 Specimens and measurements

Three mortar specimens (named Snorm, SCaCO3, and Sblack) were prepared. Snorm is a normal mortar specimen without discoloration (Fig. 1(a)). In contrast, the surface of  $S_{CaCO3}$  is covered with calcium carbonate, simulating the occurrence of efflorescence (Fig. 1(b)); the specimen was prepared by pouring calcium carbonate aqueous solution over the mortar surface and drying it at room temperature. The S<sub>black</sub> is a specimen prepared as a reference (Fig. 1(c)), and its surface was coated with black-body paint (TA410KS, ICHINEN TASCO Co., LTD.). Each specimen was 38 mm and 5.6 mm in diameter and thick, respectively. The surface spectral absorptivity of these specimens was measured in the visible (400-900 nm), short wavelength (1350-2500 nm), and medium/long wavelength (2500-12000 nm) ranges (note that the division of the infrared bands in this study was determined by referencing the manual book of the infrared camera used in the following experiments [34]). The spectrometers for the measurement of the visible, short, and medium/long wavelength ranges were FLAME-S-UV-VIS-ES (Ocean Insight Inc.), NeoSpectra-Micro (Si-Ware Systems Inc.), and FT-IR 680-IR (Agilent Technologies Inc.), respectively. All the measurements were performed using the diffuse reflectance method (basically similar to diffuse geometry, specular component included (8:di) [35]). Subsequently, the measured spectral absorptivity of S<sub>norm</sub> and S<sub>CaCO3</sub> were normalized by that of S<sub>black</sub> to obtain the relative absorptivities  $(A_r)$  of  $S_{norm}$  and  $S_{CaCO3}$  assuming the spectral absorptivity of the  $S_{black}$  as 100%.



Fig. 1 Mortar specimens used for measurement of spectral absorptivity: (a) S<sub>norm</sub>, (b) S<sub>CaCO3</sub>, and (c) S<sub>black</sub>.

#### 2.2 Measurement results

The measured relative absorptivities  $A_r$  of the  $S_{norm}$  and  $S_{CaCO3}$  specimens are presented in Fig. 2 (the vertical axis in Fig. 2 indicates  $A_r$ ). The absorptivity of the  $S_{norm}$  and  $S_{CaCO3}$  specimens in the visible and short wavelength ranges were approximately 70% and 20%, respectively. The absorptivity of  $S_{CaCO3}$ , which simulates the discoloration caused by efflorescence, was significantly smaller than that of  $S_{norm}$ . This means that using light in the visible/short wavelength range is inefficient for the active thermography inspection of surface-whitened mortars. In contrast, the absorptivity of  $S_{norm}$  in the wavelength range greater than 8000 nm was approximately 100%, and that of  $S_{CaCO3}$  was 70–80%. This indicates that long wavelength light is suitable for the inspection of mortars, including discolored mortar.



Fig. 2 Relationship between surface absorptivity Ar of Snorm and SCaCO3 specimen and wavelength

of incident light (solid lines). Circle and cross plots represent the results of the experiments in Sections 3 and 4, respectively.

# 3. Relationship between heating efficiency and wavelength of heating light

The specimens presented in Fig. 1 were heated using three different wavelength ranges (visible, short, and medium/long wavelength ranges), and the difference in heating efficiency caused by the different wavelength lights was compared with the results of the surface spectral absorptivity.

## 3.1 Experimental setup

Figure 3(a) shows the experimental setup using visible light, which was heated using a 500 W halogen lamp with an optical short-pass filter (< 900 nm, HA50, HOYA Co., Ltd.). Halogen lamps emit light in a broadband wavelength range from visible to approximately 3,500 nm [36]. Thus, by filtering the light from the halogen lamp, only visible light is selectively emitted. For the experiment in the short wavelength range, two filters (short-pass filter; SP-1600, IR-System Co., Ltd., and long-pass filter; IR85N, HOYA Co., Ltd.) were placed between the specimen and the halogen lamp to limit the wavelength range to 850-1600 nm (Fig. 3(b)). Experiments in the long wavelength range were performed using 46 W CO<sub>2</sub> laser equipment (Multiscan VS, Rofin-Baasel, Inc.); the wavelength of the CO<sub>2</sub> laser was 10600 nm (Fig. 3(c)). The emitted laser beam had a focal point at the distance of 147 mm from the laser head and expanded as the heating distance becomes farther than the focal distance. In the experiment, the specimens were placed at approximately 1 m away from the laser head; at this distance, the expanded laser beam covered nearly whole surface of the specimens. The specimens were heated for 100 s using visible and short wavelength light. When a CO<sub>2</sub> laser was used, the specimens were heated for 1.6 s because the heating power of the CO<sub>2</sub> laser was much larger than that of visible/short wavelength light. In the experiments, the temperature increases in the non-heated surface (i.e., the rear surface, not the heated surface) of the specimens were observed using an infrared camera (A315, Teledyne FLIR LLC); the infrared camera was equipped with  $320 \times 240$  uncooled microbolometer detectors with a detectable wavelength range of 7.5–13 µm. The distance between the specimen and camera was approximately 300 mm, and the observed back surface of the specimens was coated with blackbody paint. The temperatures were observed not only during heating but also after heating. The total observation times were 140 s and 60 s for visible/short wavelength light heating and CO<sub>2</sub> laser heating, respectively.



Fig. 3 Schematic of the experimental setup when specimens are heated using light with a wavelength of (a) visible, (b) short wavelength, and (c) long wavelength ranges.

## 3.2 Results

The temperature increases of the three specimens observed when each wavelength of light was used are presented in Fig. 4. It is worse noting that the temperatures obtained when using CO<sub>2</sub> laser (Fig. 4(c)) were similar to the temperature curves obtained when measuring thermal diffusivity using Parker's method [37] because the heating duration of laser heating was much shorter than that of halogen lamp heating. To compare the observed temperature increases with the spectral absorptivities presented in Fig. 2, the relative temperature increases ( $T_r$ ) of  $S_{norm}$  and  $S_{CaCO3}$  were obtained by normalizing these temperatures by those of  $S_{black}$  (thus, in the  $T_r$  values, the influence of differences in the surface absorption properties was reflected). The obtained  $T_r$  values are presented in Fig. 5. In this figure, the scales on the horizontal axes agree with those in Fig. 4; the noisy data observed immediately after the start of heating was caused by the small temperatures in early stage (see in Fig. 4). Figure 5 shows that  $T_r$  obtained when using the CO<sub>2</sub> laser is larger than that obtained when visible or short wavelength light is used. In addition, the difference between the  $T_r$  of  $S_{norm}$  and  $S_{CaCO3}$  (i.e., the reduction in  $T_r$  due to discoloration) is the smallest when using the CO<sub>2</sub> laser. These results show that long wavelength light is effective for heating mortars, including discolored mortars owing to efflorescence.  $T_r$  values in each wavelength range are presented in Fig. 2 as open circles. The plotted  $T_r$  values were determined as the average of the values for 110–140 s in Fig. 5(a) and (b) (visible and short wavelength ranges) and for 30–60 s in Fig. 5(c) (long wavelength range). These results indicate that  $T_r$  at each wavelength agrees with the spectral absorptivity  $A_r$ . This implies that the heating efficiency is correlated with the surface spectral absorptivity.



Fig. 4 Experimentally observed temperature increases for three specimens when using (a) visible light (< 900 nm), (b) short wavelength light (850–1600 nm), and (c) CO<sub>2</sub> laser (10600 nm).



Fig. 5 Relative temperature increases  $T_r$  obtained by normalizing temperatures (in Fig. 4) of  $S_{norm}$ and  $S_{CaCO3}$  by that of  $S_{black}$  when using (a) visible light, (b) short wavelength light, and (c) CO<sub>2</sub> laser.

## 4. Inspection of mortar specimens with an artificial defect

The relationship between the heating efficiency and the surface spectral absorptivity, which depends on the wavelength of the heating light, was investigated in the previous section. Meanwhile, the inspection capability of active thermography depends on the heating efficiency. Thus, the inspection capability should also depend on the wavelength of the heating light. In this section, the inspections of specimens with artificial defects were performed using heating lights with different wavelengths, and the defect detection capabilities were compared.

#### 4.1 Experimental setup

Figures 6 (a)–(c) show the photographs of the three mortar specimens and Fig. 6(d) shows a schematic of the specimens. The specimens were 85 mm  $\times$  100 mm  $\times$  55 mm and had an insertion of polystyrene foam with a thickness of 5 mm as an artificial defect (the polystyrene foam insertion was used to simulate an air gap in mortars because of its low density and thermal conductivity similar to those of air). The defect width and depth from the heated surface were 30 mm and 5 mm, respectively. The surface conditions of the specimens were the same as those shown in Fig. 1 (S<sub>norm</sub>, S<sub>CaCO3</sub>, and S<sub>black</sub>). The specimens were heated using the same halogen lamp or CO<sub>2</sub> laser described in the previous section. Unlike the experiments in the previous section, the halogen lamp was equipped with no filters to input enough heat to the specimen; thus, the input light had wavelengths in both the visible and short wavelength ranges (the spectral absorptivity of visible and short wavelength light were similar, as shown in Fig. 2). In these experiments, the heater and infrared camera were placed on the same side, and the temperature of the heated surface was monitored using an infrared camera (i.e., single-side reflection inspection was performed because it is the most frequently used active thermography inspection method). In halogen lamp heating, the specimens were heated for 100 s and cooled in the air for 40 s; the surface temperatures were observed for total 140 s (both during heating and cooling). In contrast, when using the CO<sub>2</sub> laser, the heating and cooling duration were approximately 10 and 60 s, respectively; only the temperature during cooling was observed in order to protect the infrared detector from the scattered laser during heating. Thermal images were obtained using the same infrared camera used in Section 3 with a sampling frequency of 3.75 Hz. The distance between the infrared camera and the specimens was 300 mm. From the observed thermal images of each specimen, the temperature difference  $\Delta T$  between the defective and non-defective areas was obtained, and the relative temperature difference  $\Delta T_r$  of  $S_{norm}$  and  $S_{CaCO3}$  was obtained by normalizing the  $\Delta T$  of  $S_{\text{norm}}$  and  $S_{\text{CaCO3}}$  by that of  $S_{\text{black}}$ . The  $\Delta T_{\text{r}}$  values were also compared with  $A_r$  presented in Fig. 2.



Fig. 6 Photographs of mortar specimens with an artificial defect (a) S<sub>norm</sub>, (b) S<sub>CaCO3</sub>, (c) S<sub>black</sub>, and (d) schematic of the specimens.

4.2 Results

The thermal images observed when using the halogen lamp and the CO<sub>2</sub> laser are presented in Figs. 7 and 8, respectively. In each image, the defective area (surface above the polystyrene foam insertion) was detected as hotter than the non-defective area, and the temperature difference  $\Delta T$  of  $S_{CaCO3}$  looks smaller than that of  $S_{norm}$  and  $S_{black}$ . The obtained  $\Delta T$  and  $\Delta T_r$  of the three specimens as a function of time are presented in Figs. 9 and 10, respectively. Figure 10 shows that  $\Delta T_{\rm r}$  obtained when using the CO<sub>2</sub> laser was larger than that obtained when the halogen lamp was used; when using the CO<sub>2</sub> laser,  $\Delta T_r$  reaches approximately 100% for  $S_{\text{norm}}$  and was approximately 60% for  $S_{CaCO3}$ . The obtained  $\Delta T_r$  values of  $S_{norm}$  and  $S_{CaCO3}$  (determined as the average of the values for 110-140 s and 40-70 s, respectively) are plotted as cross plots in Fig. 2. It should be noted that because the observed surface was the same as the heated surface in these experiments, the change in surface emissivity also affected the observation by the infrared camera [38–40]. From the results in Fig. 2, the average spectral absorptivity of  $S_{\text{norm}}$  and  $S_{\text{CaCO3}}$  in the wavelength range of  $7.5-13\mu m$ , which is the detectable wavelength range of the camera used, is approximately 100% and 86%, respectively. Thus, for comparison with  $A_r$  in Fig. 2, when estimating the  $\Delta T_r$ values of  $S_{CaCO3}$ , the results in Fig. 10 are multiplied by 100/86. By comparing the  $\Delta T_r$  values with  $A_{\rm r}$  in Fig. 2, it is found that the temperature difference observed in the defective area has a clear correlation with Ar. These results demonstrate that defects in mortars, including discolored mortars, can be detected efficiently using light with wavelengths in the long wavelength range.



Fig. 7 Thermal images at 140 s obtained when using a halogen lamp for mortar specimen (a) S<sub>norm</sub>,(b) S<sub>CaCO3</sub>, and (c) S<sub>black</sub>.



Fig. 8 Thermal images at 60 s obtained when using CO<sub>2</sub> laser for mortar specimen (a) S<sub>norm</sub>, (b) S<sub>CaCO3</sub>, and (c) S<sub>black</sub>.



Fig. 9 Experimentally observed temperature difference  $\Delta T$  between the defective and nondefective areas for three specimens when using (a) halogen lamp and (b) CO<sub>2</sub> laser.



Fig. 10 Relative temperature difference  $\Delta T_r$  obtained by normalizing  $\Delta T$  of  $S_{norm}$  and  $S_{CaCO3}$  by that of  $S_{black}$  when using (a) halogen lamp and (b) CO<sub>2</sub> laser.

### 5. Conclusions

In this study, the surface spectral absorptivity of mortars discolored by the occurrence of CaCO<sub>3</sub> efflorescence was measured, and the effective heating light wavelengths for active thermography inspection of the discolored mortars was investigated. Spectroscopic measurements revealed that the surface spectral absorptivity of mortars significantly increased at a wavelength of approximately 3000 nm regardless of the presence/absence of the discoloration; the absorptivity in the long wavelength range was higher than that in the visible/short wavelength range. Experiments using optical light with three different wavelength ranges showed that the heating efficiency and defect detection capability (temperature difference observed in the defective region) correlate with the surface spectral absorptivity. The defects in the discolored specimen were detected more efficiently when using a CO<sub>2</sub> laser (light in the long wavelength range) than when using a halogen lamp (visible/short wavelength light). These results indicate that, although long wavelength light is conventionally known to be easily absorbed by concretes, it is also suitable for heating mortars whose surface is covered with calcium carbonate, and that using long wavelength light is an effective method for enhance the inspection capability of active thermography inspection of surface-whitened mortars.

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measured at Tokyo Metropolitan Industrial Technology Research Institute.

### **Authors' contributions**

Masashi Ishikawa conceptualized the study, conducted the experiments, and wrote the main manuscript text, Akira Emoto designed the experiments and interpreted the results, Yoshihiro Suto conducted experiments and prepared figures, and Hideo Nishino supervised and evaluated the results. All authors reviewed the manuscript.

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#### Availability of data and material

The datasets generated during and/or analyzed during the current study are available from the corresponding author on reasonable request.

# Declarations

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Not applicable.

Competing interests:

The authors declare that they have no competing interests.

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